

1 **Renewable energy from thermophilic anaerobic digestion of winery**
2 **residues: batch and CSTR lab-scale study**

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10 **Abstract**

11 Winemaking process generates many by-products, mainly grape marcs, grape stalks and wine lees.
12 Large amounts of wastewater are also produced.

13 Anaerobic digestion is considered particularly suitable to treat winery wastes because of their high
14 organic matter content with respect of nutrients and for the interesting energetic potential, but to
15 date only mesophilic process was investigated. In this study potential methane production and
16 kinetic constants were determined by batch trials at thermophilic condition, and compared with
17 mesophilic ones. Grape marcs appeared the most interesting substrates with an estimated potential
18 higher than $0.3 \text{ Nm}^3\text{CH}_4/\text{kgVS}_{\text{fed}}$. In order to assess the feasibility of the continuous process a lab-
19 scale semi-continuous reactor was setup. Because of the consumption of buffer capacity, the
20 biological process was hard to control, on the other hand, an interesting production was obtained
21 with HRT of 40 days and with previous fermentation of grape marcs ($0.29 \text{ Nm}^3/\text{kgVS}_{\text{fed}}$). The
22 results were used to calculate the potential energy recovery from grape marcs in a full-scale
23 application, in terms of heat and electricity: 245 GWh/y of heat and 201 GWh/y of electricity in
24 different scenarios.

25

26 **Keywords**

27 Anaerobic digestion; winery waste; renewable energy; BMP test; grape marcs.

28 **1. Introduction**

29 The International Organization of Vine and Wine (OIV) estimated a global wine production of
30 278.6 Mhl in 2013 (OIV, 2014). Italy, France and Spain are the countries with the highest
31 productions (131.6 Mhl), and together with others European countries account for about 59% of
32 world production.

33 In Europe wineries have a long tradition and high economic relevance in the agricultural sector, on
34 the other hand, with their activity they also determine a considerable environmental footprint:
35 intensive use of soil, introduction on the environment of pesticides and heavy metals, water
36 consumption, production of high quantities of co-products and wastes (Bolzonella and Rosso,
37 2009).

38 In early 2000s the Italian Agency for Environmental Protection (ANPA, 2001) evaluated the
39 amount of winery waste (WW) for each hectolitre of wine produced, considering different type of
40 cellars in terms of dimensions and location. The production of wastewater is typically 2hl for each
41 hl of wine produced, but it depends on process technology and can reach 6 hl per hl of wine (Berta
42 et al., 2003). The wastewater is usually treated by conventional activated sludge processes and the
43 sludge obtained is about 1kg of dry matter per hl of wine (ANPA, 2001). Sludge, generally, could
44 not be spread on land for agricultural purpose cause of its high heavy metals content and low
45 biological stability: this means high management and disposal costs (110€/ton).

46 Grape stalks and marcs, wine lees, exhausted grape marcs and vinasses are the main by-products
47 generated by the wine and alcohol-producing industries (Bustamante et al., 2007). The productions
48 of solid by-products and wastes were estimated of 4 kg of grape stalks, 18 kg of grape marcs and 6
49 kg of wine lees per hl of wine produced. The European Council Regulation (EC) 1493/1999 of the
50 common organization of the wine market introduced compulsory distillation of wine by-products,
51 including grape marcs and lees, to produce spirits, alcohol, tartaric acid, exhausted grape marcs and
52 liquid waste (vinasses). The aim of this practice was to avoid over-pressing of marcs and to
53 maintain high quality wine markets, but not to reduce the polluting hazard of winery waste disposal.
54 Distilleries received a subsidy to distil the alcohol for industrial and energy uses but, on the other
55 hand, disposal of marcs via distillation was becoming a considerable financial and bureaucratic
56 burden for wine producers. In fact, although the distilleries paid a small amount for the marcs, the
57 producers had to pay for the cost of transport. As a result, producers were not only being
58 constrained to waste potentially useful by-products but also the transport cost was higher than price
59 paid by the distillery.

60 Recently the market-protective legislation (EC 479/2008 and EC 555/2008) allowed alternative uses
61 of grape marcs in the wineries (Krzywoszynska, 2013) and granted more autonomy for marcs
62 management strategy. In Italy, since 2011 (DM 27/11/08) marcs could be distilled or utilized by

63 producers in other ways (under supervision of environmental control bodies) such as anaerobic
64 digestion, pyrolysis or incineration, spreading on agricultural land (raw or composted) according to
65 local legal framework of course, or as a raw material for cosmetics and pharmaceuticals production.
66 Alternative technologies to reuse WW are the extraction and recovery of polyphenolic compounds,
67 the production of grape seed oil, fermentation to produce lactic acid and laccase (Arvatoyannis et
68 al., 2008).

69 The use of raw solid winery waste for agricultural purpose is an hazardous practice because the high
70 organic content could consume high quantity of oxygen in the soil, then establishes anoxic
71 conditions. As reported by Moraes et al. (2014), the impacts caused by potential greenhouse gas
72 emissions resulting from organic matter degradation on soil, the unpleasant smells generated and
73 possibility attracting insects should be considered. The presence of polyphenols, compounds related
74 to phytotoxic and antimicrobial effect, and low pH due to high concentration of organic acids such
75 as tartaric, citric and malic acids, make their treatment and disposal indispensable and their
76 management really difficult. Biological treatment could be a solution, increasing the biological
77 stability and improving COD/N/P ratio. Among the available technologies, composting of winery
78 solid organic waste can produce a good quality fertilizer (Bertan et al., 2004) but it must be taken
79 into account the costs related to the energy required for pile handling and venting (Bonifazi et al.,
80 2013). Moreover winery wastes had nutrients ratio unbalanced for aerobic degradation, caused by a
81 low nitrogen and phosphorus content.

82 Another biological treatment is Anaerobic Digestion (AD), a particularly suitable treatment to
83 stabilize winery waste (Moletta et al., 2005) even at low level of nitrogen and phosphorus and it can
84 remove organic pollutant such as polyphenols. This technology is considered an important future
85 contributor to the energy supply of Europe (Appels et al., 2008) and the WW represents a consistent
86 raw material. The appropriate use of biogas for energy generation may also reduce GHG emissions
87 because it would avoid the release of biogenic CH₄ in the atmosphere (Moraes et al., 2014).

88 ~~Several authors reported positive cases of anaerobic treatment of winery wastewater, using process
89 with micro-organisms in biofilm structures and low influent suspended solids concentration such as
90 UASB, MBBR, hybrid USBF (Andreottola et al. 2009; Sheli et al., 2007; Molina et al., 2007).~~

91 Completed stirred tank reactors (CSTR) were preferred when the semi-solid waste, such as grape
92 marcs (GM), grape stalk (GS) and wine lees (WL), were treated. The OLR applied to AD was lower
93 than in above-mentioned technologies, the HRT usually was higher than 12 days to avoid wash-out
94 of methanogens microorganisms and to increase the hydrolysis rate.

95 Lots of examples of AD of WW were reported in literature but all trials were carried out in
96 mesophilic condition, with temperature from 37°C to 40°C. In the most cases batch mode was

97 applied, then the results were the potential methane production obtained from best operational
98 conditions. The range of results was wide due to several factors: inoculum characteristics and
99 substrate to inoculum ratio (VS basis) determined the answer of microorganisms to new substrates
100 (Rebecchi et al., 2013), in fact winery waste can contained substances, such as lignin, ethanol and
101 polyphenols, that are not present in the animal effluents, sewage sludge and bio-waste; also
102 variability of substrates characteristics determined different biogas productions (Fabbri et al.,2014;
103 Lo et Liao, 1986) and was usually linked to the type and the origin place of grape and to the wine-
104 making processes that generate them. For example Fabbri et al. (2014) reported that best
105 biomethane potential was achieved by a white grape marc ($0.273 \text{ m}^3\text{CH}_4/\text{kgVS}$) while the red one
106 reached $0.101 \text{ m}^3 \text{CH}_4/\text{kgVS}$. Anaerobic digestion of grape marcs is the more investigated process:
107 the specific production ranges from 0.076 to $0.283 \text{ m}^3\text{CH}_4/\text{kgVS}_{\text{fed}}$ (Failla et al., 2009; Dinuccio et
108 al., 2010; Gunaseelan et al., 2003). Specific methane production of grape stalk ($0.098 - 0.180$
109 $\text{m}^3\text{CH}_4/\text{kgVS}_{\text{fed}}$) is lower than other agro-industrial biomasses probably due to high lignin content
110 (23.3% of solids), that cannot be degraded in anaerobic conditions (Angelidaki et al., 2000; Ward et
111 al.,2008). Few authors studied the wine lees (WL), although the potential methane is very high in
112 terms of biogas produced and methane content (Lo and Liao, 1986; Da Ros et al., 2014); this
113 probably because of the low quantity of WL that could be recovered (6 kg each hl of wine
114 produced). Moreover there are many typologies of lees, different for kind of fining agents, such as
115 bentonite, gelatine, albumin or activated carbon, added in order to settle suspended solid and
116 colloidal particles. Sometimes wineries recovery must or wine in the lees by centrifugation or
117 filtration through filter medium consist of diatomaceous earth or perlite (Setti et al., 2009). In these
118 cases at the end of recovery operation the lees are composed by the filter medium plus the lees
119 itself, so the final lees have high concentration of inert material.

120 Generally the greater difficulty found in AD of WW was the control of pH in the reactor, in fact the
121 abundance of organic acids caused the rapid formation of volatile fatty acids (VFA) and the drop in
122 pH (Lo and Liao, 1986). Limited buffer capacity was partially due to low nitrogen content in
123 substrates and it was usually supplied by adding NaOH solution (Sheli et al., 2007, Melamane et al.,
124 2007) but the use of chemicals reduces the economic revenues of the process. A solution to increase
125 ammonium content and alkalinity in the anaerobic reactors is to introduce organic waste from others
126 agro-industrial sectors. Anaerobic co-digestion (AcoD) with manure or waste activated sludge
127 allows to reach C/N ratio more favourable, and consequently the biogas production and removal
128 efficiency increase (Riaño et al.,2011; Rodriguez et al., 2007; Soldano et al., 2009).

129 The results of cited studies were mainly obtained by mesophilic process ($35\text{-}40^\circ\text{C}$), while
130 thermophilic condition was less applied (Da Ros et al., 2014, Rebecchi et al., 2013). Increasing

131 temperature at 55°C has several benefits: improves solubility of the organic compounds and
132 depletion of pathogens (Sahlström, 2003), enhances biological and chemical reaction rates
133 (Cavinato et al. 2013, Cecchi et al. 1991). However, the application of high temperatures has some
134 disadvantages: the higher free ammonia fraction, which plays an inhibiting role for the
135 microorganisms, and the pK_a change of the VFAs that makes the process more susceptible to
136 inhibition (Appels and al., 2008). In both the above cited thermophilic anaerobic digestion of
137 winery waste studies, process instability was observed with VFAs accumulation and pH drop. In
138 particular Rebecchi et al. (2013) found results lower than mesophilic ones and continuous process
139 was not investigated, on the other hand some studies (Da Ros et al., 2014; Riaño et al., 2011)
140 described trials carried out using a co-substrate and didn't evaluate potential biogas production of
141 sole winery waste in the optimal conditions.

142 The aim of this work was to supply the information on thermophilic anaerobic digestion of winery
143 solid waste and in particular of grape marcs, both in batch and continuous mode. Batch test were
144 carried out according with guidelines of Angelidaki et al. (2009) with different wastes, obtaining
145 preliminary results about biogas productions and they were compared with mesophilic methane
146 production and few existing data at 55°C. Empirical linear and non-linear regression models were
147 developed to evaluate digestion performance and to compare mesophilic and thermophilic process
148 in terms of kinetics parameters. However, it is well known as biogas yields, under semi-continuous
149 flux condition can be different from those observed under batch conditions, then semi-continuous
150 trials in lab-scale were carried out to determine best operational conditions and to highlight
151 criticisms treating grape marcs. Economical and energy aspects are than evaluated considering a
152 potential full-scale application.

153 **2. Materials and Methods**

154 2.1 Winery wastes

155 The winery by-products considered in this study were grape marcs (GM), grape stalks (GS) and
156 wine lees (WL). Two type of GM were considered: virgin grape marc (VGM) and grape marc after
157 a natural fermentation (FGM). Samples were collected in a cellar in the north-east of Italy and each
158 waste stream were labelled and stored in a freezer at -20°C until required. These substrates were
159 analyzed in triplicate in terms of total and volatile solids, chemical oxygen demand (COD), total
160 Kjeldahl nitrogen (TKN) and total phosphorus, according to the Standard Methods (2012).

161

162 2.2 BMP tests

163 The biogas production was determined using biochemical methane potential tests (BMP) at 55°C.
164 The inoculum digestate was collected from a full-scale digester (Treviso WWTP) treating organic
165 fraction of municipal solid waste and waste activated sludge at mesophilic temperature. Inoculum
166 had an average solid concentration of 43.1 gTS/kg, with 67% volatile solids. The particulate COD
167 was 928 mg/gTS, while nitrogen and phosphorus were present respectively with 16.1 and 7.8
168 mg/gTS. For each waste considered different substrate to inoculum ratio were tested, ranged from
169 0.04 to 0.40 $\text{gVS}_{\text{substrate}}/\text{gVS}_{\text{inoculum}}$ in order to evaluate possible inhibition effect. BMP tests of the
170 inoculum alone (blank) were also conducted. The results were expressed at standard conditions for
171 temperature and pressure (0°C and 1 atm), and the unit of specific methane production (SMP) was
172 $\text{Nm}^3\text{CH}_4/\text{kgVS}_{\text{fed}}$. The average methane yield from the blanks was subtracted from the yields of
173 tested samples, in order to accurately assess the BMP yields.

174 The COD content of winery wastes and the theoretical methane production on COD basis (0.350 m^3
175 CH_4/gCOD by stoichiometric conversion reaction) were used to calculate the theoretical maximum
176 methane potential from each substrate, and the biodegradability index was calculated considering
177 the ratio between the measured and the theoretical methane production.

178 Two first order kinetic models were used to fit the cumulative methane production data from the
179 BMP tests. Assuming first-order kinetics for the hydrolysis of particulate organic matter, the
180 cumulative methane production can be described by the kinetic equation (1):

$$181 \quad \quad \quad 182 \quad \text{BMP} = \text{BMP}_{\infty}(1 - \exp(-kt)) \quad (1)$$

183
184 where BMP is the cumulative methane yield at digestion time t days ($\text{ml CH}_4/\text{g VS}_{\text{fed}}$), BMP_{∞}
185 methane potential of the substrate ($\text{ml CH}_4/\text{g VS}_{\text{fed}}$), k is methane production rate constant (first
186 order disintegration rate constant) (d^{-1}), t is the time (d). The duration of the lag phase is also an
187 important factor in determining the efficiency of anaerobic digestion. The lag phase can be
188 considered with the modified Gompertz model as described in Eq. (2):

$$189 \quad \quad \quad 190 \quad \text{BMP} = \text{BMP}_{\infty} \exp \left\{ - \exp \left[\frac{R_{\max} e}{\text{BMP}_{\infty}} (\lambda - t) + 1 \right] \right\} \quad (2)$$

191
192 where R_{\max} is the maximum methane production rate ($\text{l CH}_4/\text{kg VS d}$), $e = 2.7183$ and λ is the lag
193 phase for methane production to begin (d).

194 As Browne et al (2014) suggested, a nonlinear least-square regression analysis was performed using
195 Excel to determine the equations parameters (k , R_{\max} , λ) and the predicted methane yield. The

196 predicted methane yield obtained from the regression analysis was plotted with the measured
 197 methane yield. The statistical indicators, correlation coefficient (R^2) and root mean square error
 198 (RMSE) were calculated to assess the goodness of fit and evaluate the best kinetic equation to
 199 describe WW biogas production.
 200

201 2.3 Continuous AD trials

202 The BMP tests estimated the potential methane production while semi-continuous tests allowed to
 203 evaluate the feasibility of the process. Continuous trials were carried out in a lab-scale CSTR
 204 maintained at temperature of 55°C in a controlled oven. The system was inoculated with the same
 205 mesophilic digestate sludge used for BMP tests. The temperature was increased by one temperature
 206 step strategy, passing in a very short time from mesophilic to thermophilic condition as suggested
 207 by Cecchi et al. (1993). Biogas flow was measured using a MilliGascounter® (Ritter) and the gas
 208 was collected in a Tedlar gas bag to analysed its composition (CH_4 , CO_2) by gas chromatography
 209 equipped with HP-Molesieve column (30m×0.3mm×0.25µm film thickness) and a thermal
 210 conductivity detector (TCD).

211 The grape marcs were used as main substrate because of its availability and potential BMP. The
 212 reactor was fed once a day with substrate and tap water to reach the correct flow rate. Different
 213 operational conditions were tested in terms of feeding substrate, HRT and OLR, dividing the tests in
 214 four RUNs, as reported in Table 1.
 215

Table 1 Operational conditions of semi-continuous trials

	Feed	Organic loading rate (kgVS/m ³ d)	HRT (d)
RUN1	Grape marcs	1.0	20
RUN 2	Grape marcs	2.0	20
RUN 3	Grape marcs + Activated Sludge	4.0	20
RUN 4	Fermented Grape marcs	1.2	40

216
 217 Partial and total alkalinity (PA and TA), pH, VFA, ammonium nitrogen were measured twice a
 218 week to monitor the process stability, while the characteristics of the effluent in terms of total and
 219 volatile solids, COD, TKN and total phosphorus (P_{tot}) were analyzed weekly. All the analyses,
 220 except for VFA, were carried out in accordance with the Standard Methods (APHA, 2012). Volatile
 221 fatty acids content was monitored using a gas chromatograph (Carlo Erba instruments) with
 222 hydrogen as gas carrier, equipped with a Fused Silica Capillary Column (Supelco NUKOLTM,

223 15m×0.53mm×0.5 μm film thickness) and with a flame ionization detector (200°C). The
224 temperature during the analysis started from 80°C and reaches 200°C through two other steps at 140
225 and 160°C, with a rate of 10°C/min. The analyzed samples were centrifuged and filtrated on a 0.45
226 μm membrane.
227

228 3. Results and Discussion

229 3.1 Characterization of winery waste samples.

230 The characteristics of substrates tested in trials are reported in Table 2. The results reflected typical
231 characteristics of WW: total solids ranging from 225 to 430 gTS/kg, of which about 90% were
232 volatile solids. WL had low volatile solids content, because during the winemaking process
233 diatomaceous earth, that is an inert material, was used in order to remove suspended solids and
234 colloidal particles. The COD in the WW was higher than 1,000 mgO₂/l, except for WL, but part of
235 organic matter was lignin and cellulose (Dinuccio et al., 2010).

236 During the experimentation waste activated sludge (WAS), collected in cellar wastewater treatment
237 plant, was used. The sludge was derived from biological nutrient removal process working with a
238 solid retention time of 15 d and food to microorganisms ratio of 0.15 kg COD/kg MLVSS d. The
239 WAS had 45.4 gTS/kg with 60% of volatile solids. The concentrations of COD, TKN and P_{tot} were
240 921 mgCOD/gTS, 31.4 mgN/gTS and 7.0 mgP/gTS respectively, corresponding with COD:N:P
241 ratio of 132:4:1.
242

Table 2 Chemical-Physical characteristics of analyzed winery wastes

Parameters	Unit	GS	Virgin GM	Fermented GM	WL
TS	g/kg _{ww}	226.8± 40.8	371.0 ± 51.9	425.2 ± 21.3	289.5 ± 5.8
VS	g/kg _{ww}	201.7 ± 54.5	334.1 ± 30.1	383.4 ± 30.7	114.6 ± 4.6
COD	mg O ₂ /gTS	1,306 ± 131	1,078 ± 32	1,132 ± 68	352 ± 46
TKN	mgN-NH ₄ ⁺ /gTS	6.1 ± 1.0	20.4 ± 0.8	16.8 ± 4.5	15.0 ± 2.4
P _{tot}	mgP-PO ₄ ³⁻ /gTS	3.6 ± 1.8	5.5 ± 4.1	1.2 ± 0.3	0.8 ± 0.4

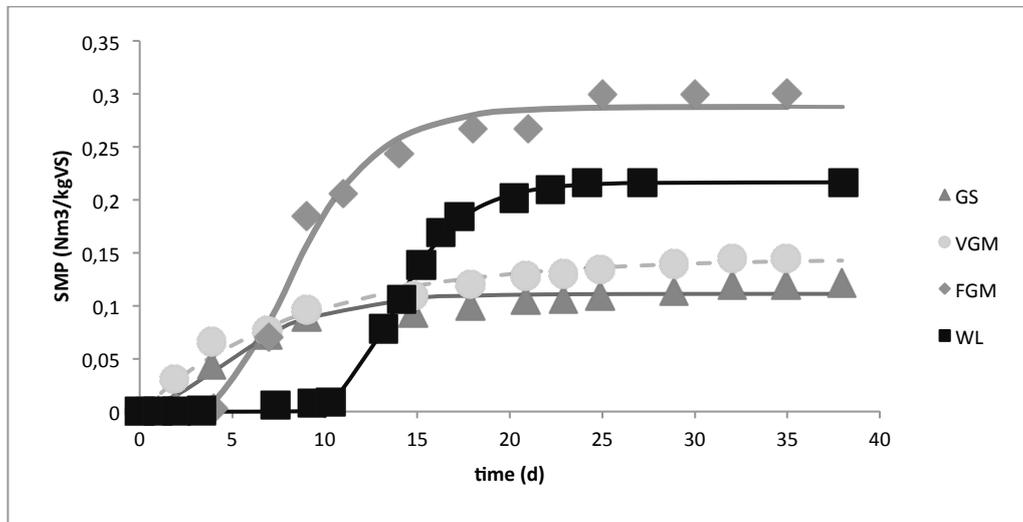
243

244 3.2 Methane production in batch trials

245 The specific methane production (SMP) values were measured for each substrate (WL, GS, virgin
246 GM and fermented GM) using the BMP tests in thermophilic condition. The Figure 1 shows the
247 cumulative average SMP from the batch experimentations. The hydraulic retention time of 30 days

248 was enough to convert the organic matter in anaerobic condition, in fact within this time the daily
249 variation of methane was lower than 5% of cumulative production.

250



251

252 Figure 1 Cumulative specific methane production of wine lees, grape stalk, virgin and fermented grape marcs at
253 thermophilic temperature. Continuous lines indicate modified Gompertz model predictions, while dotted line indicates
254 first order model prediction.

255 Specific methane production of GS was 0.121 Nm³/kgVS_{fed} the value was far from theoretical
256 methane production deriving from COD concentration (0.514 m³/kgVS_{fed}), consequently only 24%
257 of organic matter was converted into methane. The low biodegradability index was justified by data
258 reported by Dinuccio et al (2011) about high content of lignin (23% TS) that was not biodegradable
259 in anaerobic condition, and of cellulose and hemicellulose (15.9 and 23.5 %TS respectively) that
260 were partially degraded.

261 Significant differences were observed in virgin and fermented GM. The average SMP of virgin
262 grape marcs were 0.150 Nm³/kgVS_{fed} with 36% of COD conversion into methane. The production
263 value was consistent with those reported by Colussi et al. (2009). The composition in terms of
264 lignin, hemicellulose and cellulose was similar to GS and explained the low gas production. The
265 natural fermentation of GM was a pre-treatment that allow to obtain, from complex molecules,
266 rapidly biodegradable compounds, and improved methane production, in fact it reached 0.301
267 Nm³/kgVS_{fed} corresponding to biodegradability index of 68%.

268 The WL had similar conversion efficiency (70%) but SMP reached 0.216 Nm³/kgVS_{fed}; the
269 presence of readily biodegradable compounds partially inhibited the process and the
270 methanogenesis started after about 9 days.

271 Considering winery wastes biogas production reported in literature, the most evident aspect was the
272 variability in specific methane production. As demonstrated by Fabbri et al. (2014) the grape type

273 determined different biogas production also operating in same operational conditions, in fact the
 274 variation coefficient calculated for available mesophilic values for GM was about 40%, while for
 275 GS lowered to 25%. Existing result of thermophilic digestion of GM (Rebecchi et al., 2013) was
 276 discouraging ($0.04 \text{ m}^3\text{CH}_4/\text{kgTVS}$), instead this study determined methane yields in same
 277 magnitude order of mesophilic one (Table 3). Considering many available figures, comparison
 278 between mesophilic and thermophilic potentials was not easy. Average values for GM and GS,
 279 0.196 (metti anche range e riferimento alla tabella sotto) and $0.139 \text{ m}^3\text{CH}_4/\text{kgVS}$ respectively, were
 280 considered for mesophilic process. Process at 55°C reduced methane production of GS of 13%,
 281 value consistent with intrinsic variability and difficulty associable to operational temperature. The
 282 behaviour of GM depends on pre-treatment, virgin substrate was characterized by lowering of
 283 methane production of 23%, while fermented one increased of 53%. These preliminary results
 284 didn't justify possible inhibition at thermophilic temperature but probably indicated the low
 285 biodegradability of used pomace; anyway they are inside the range of literature values. The wine
 286 lees BMP appeared significantly lower than value reported by some authors (Lo and Liao, 1986;
 287 Danieli and Aldeovandi, 2011) mainly due to different origin process. Overall, the thermophilic AD
 288 in batch reactor didn't significantly increase biogas production compared to mesophilic test.

289 Table 3 Comparison of biogas and methane production reported in literature and in this study (* indicates value
 290 obtained by continuous process, bold data refer to thermophilic process)

Substrate	Temperature	Specific production			CH ₄	References
	°C	m ³ biogas/ kgTVS	m ³ CH ₄ / kgTVS	m ³ CH ₄ / kgCOD	%	
GS	40	0.225	0.098		44	Dinuccio et al., 2010
	35		0.18			Gunaseelan, 2003
	35-37	0.297	0.14			Fabbri et al 2014
	55		0.121			This study
GM	40	0.25	0.116		46	Dinuccio et al., 2010
	35		0.283			Gunaseelan, 2003
	40	0.120-0.159	0.096-0.128		80-81	Faila and Restuccia., 2009
	35		0.15			Colussi et al., 2009
	35			0.147		Fountolakis et al., 2008 *
	35-37	0.406	0.273		67.32	Fabbri et al 2014
	35-37	0.322	0.157		48.71	Fabbri et al 2014
	55		0.04			Rebecchi et al., 2013
55		0.150-0.301			This study	
WL	35		0.367-1.048			Lo and Liao, 1986
	36		0.488		60	Danieli and Aldeovandi, 2011
	55		0.216			This study

292 3.3 Kinetic study results

293 The results of the kinetics analysis using the first order kinetic model and the modified Gompertz
 294 model are summarised in Table 4. The first order kinetic model could not be applied to test WL
 295 because the result was far from real data. In the other cases the model gave similar k values for GS
 296 and VGM, and the k value of FGM was lower probably due to inhibition effect that was not
 297 consider in the model. In fact GS and GM had lower lag times determined by modified Gompertz
 298 model, while the VGM and WL had 4.7 and 10.8 days g lag phase, respectively.

299 Both models exhibited a good fit when plotted against the measured data, with a determination
 300 correlation coefficients (R^2) ranging from 0.97 to 0.99 for the first order model and from 0.98 to
 301 1.00 for the Gompertz model. The RMSE ranged from 7 to 35 mlCH₄/g VS_{fed} for the first order
 302 model while the Gompertz model gave lower values of over 8–14 mlCH₄/g VS_{fed}. The modified
 303 Gompertz model gave slightly lower predicted maximum BMP yields than the measured data
 304 ranging from -4% to -8% while the first order model generally gave higher predicted methane. The
 305 model Gompertz gave a more accurate predicted max methane yield than the first order equation,
 306 especially when lag time was observed. While if there wasn't lag phase, as in test with VGM, this
 307 model introduced a significant error with negative value of λ . Correlation coefficient and root mean
 308 square demonstrated that modified Gompertz model fitted better than first order model for the trials
 309 characterized by lag phase. On the other hand the model that better described the production of
 310 VGM was first order kinetic one.

311 Table 4. Results of the kinetics analysis using the first order kinetic model and the modified Gompertz model

Substrate	Unit	GS	VGM	FGM	WL
BMP	m ³ CH ₄ /kgVS _{fed}	0.121±0.023	0.150±0.088	0.301±0.087	0.216±0.137
Biodegradabilty index	%	24	36	68	70
<i>First order kinetic model</i>					
BMP predicted	m ³ CH ₄ /kgVS _{fed}	0.119	0.144	0.372	-
Δ BMP	%	-2%	-4%	24%	-
k	d ⁻¹	0.117	0.114	0.059	-
RMSE	m ³ CH ₄ /kgVS _{fed}	0.007	0.006	0.035	-
R²		0.99	0.99	0.97	-
<i>Modified Gompertz kinetic model</i>					
BMP predicted	m ³ CH ₄ /kgVS _{fed}	0.111	0.141	0.288	0.217
Δ BMP	%	-8%	-6%	-4%	0%
λ	d	0.9	1.8	4.7	10.9
Rmax	m ³ CH ₄ /kgVS _{fed} d	0.012	0.009	0.036	0.034
RMSE	m ³ CH ₄ /kgVS _{fed}	0.008	0.009	0.014	0.004
R²		0.99	0.98	0.99	1.00

312 Fabbri et al.(2014) applied same models to digestion performances and observed lag phases due to
313 presence of phenol, alkyl phenols and alcohols, commonly present in winery wastes. Consequently,
314 also at mesophilic temperature the best results were obtained by application of Gompertz model.

315 Comparing kinetic constants calculated in this study with those reported by Fabbri et al. (2014)
316 some interesting observations were made. Considering grape stalks digestion had different methane
317 production but equal kinetic constants, in fact the previous study reported hydrolysis rate of 0.11 d⁻¹,
318 0.011 m³CH₄/kgVS_{fed}d and no lag phase was detected. By these values thermophilic digestion of
319 lignocelluloses substrates had similar behaviour than mesophilic one.

320 GM had larger variability range, in terms of kinetic parameters both in mesophilic and thermophilic
321 studies.

322 Comparing the mesophilic results obtained by Fabbri with thermophilic of this study, it is possible
323 to observe that the higher methane production was also characterized by a lower lag phase and by a
324 greater maximum methane production rate. In particular ...confronta nelle due condizioni
325 separatamente .(0.9 d and 1.8d, at 37°C and 55°C respectively) (0.033 and 0.036 m³CH₄/kgVS_{fed}d,
326 at 37°C and 55°C).

327 On basis of these comparisons, thermophilic digestion in batch reactor appeared quite similar to
328 mesophilic one, and no inhibition effects or metabolites accumulation were observed.

329 3.4 Biogas production in lab-scale CSTR

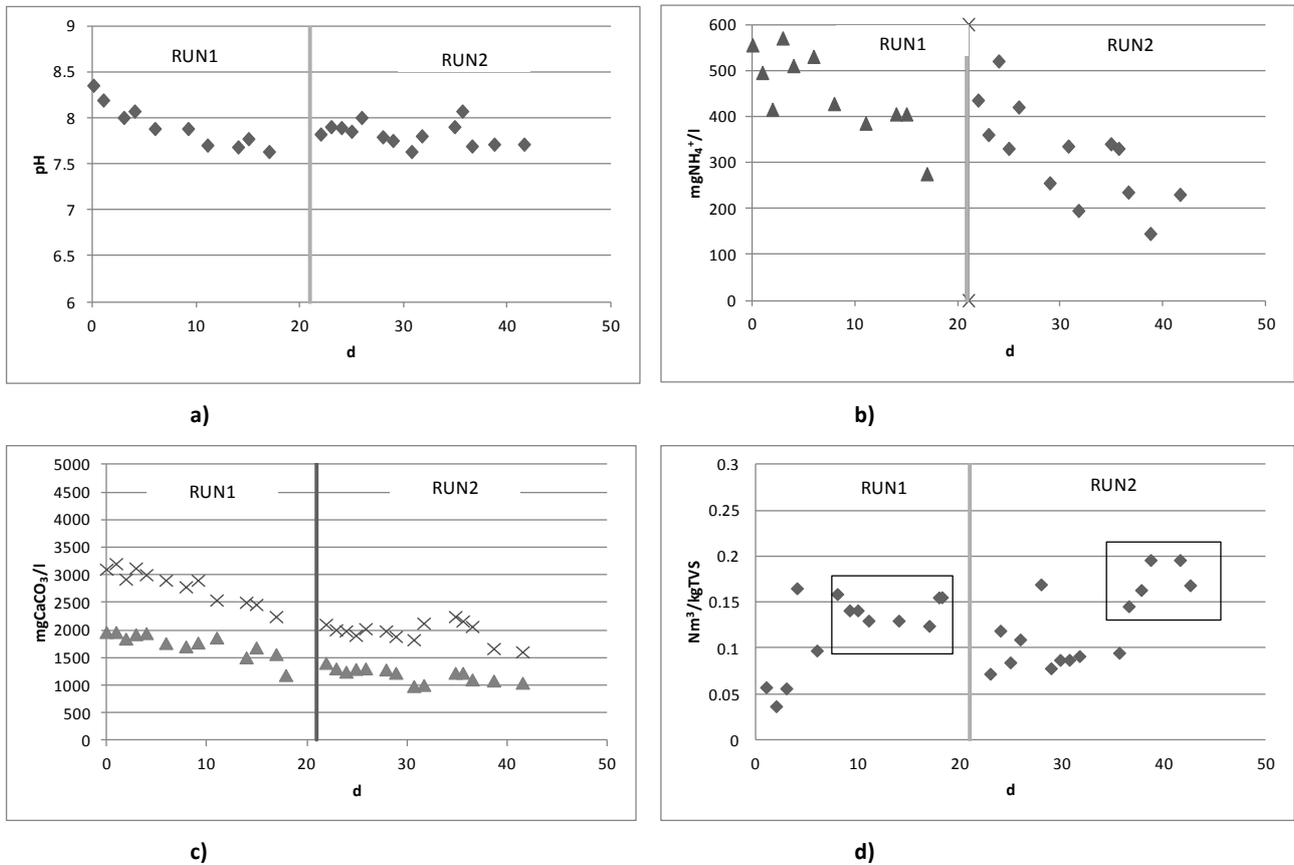
330 GM appeared the be more interesting by-product of winemaking process in terms of available
331 quantity and biogas production, so the semi-continuous tests were carried out using this substrate as
332 feeding.

333 Two trials were conducted with virgin GM alone, with organic loading rate (OLR) of 1 and 2 kg
334 VS/m³d and 20 day of HRT respectively (RUN1 and RUN2). Considering the low OLR applied the
335 process didn't need start-up and acclimatisation period. By the end of the first HRTs the system had
336 reached a steady state of methane production. The biogas production was 0.11 and 0.15
337 Nm³/kgVS_{fed} in RUN1 and RUN2 respectively, both with 75% of methane content. Considering the
338 mass balance, the volatile solid removals were of 12% and 15% respectively for OLR 1 and 2
339 kgVS/m³d.

340 Both partial and total alkalinity decreased during experimentation (Figure 2) determining a net
341 reduction of buffer capacity of the system. This eventually results in the failure of the biological
342 process although the pH value was upper 7.5. The low biodegradability index (Table 3) affected the
343 concentration of VFA that was lower than 100 mgCOD/l. The good percentage of methane and the
344 stability parameters suggested that methanogenesis was not inhibited and that hydrolysis was the

345 limiting step of the process. It was not clear if inhibition was due only to low biodegradability of
 346 substrate or if unbalance COD:N:P ratio limited the biomass growth and consequently its activity.

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351 Figure 2 Trends of pH a), ammonia b), total and partial alkalinity c) SGP d), at OLR 1 kgVS/m³d (RUN1) and 2
 352 kgVS/m³d (RUN2)

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354 In order to supply to missing nutrients and to improve stability of the process waste activated sludge
 355 from winery wastewater treatment was added as co-substrate (RUN3) because it is widely available
 356 in wine industry (Bruculeri et al., 2005). The feed was composed by 66% of virgin GM (in terms
 357 of volatile solids) and the rest derived from sludge. The total OLR applied was 4 kgVS/m³d.

358 As illustrated in Figure 3(b), the average biogas production was 0.146 Nm³/kgVS_{fed} with 50% of
 359 methane. The volatile solids removed by biogas conversion corresponded to 20%. The pH value
 360 range from 7.5 to 8, without considerable variation during the test, while the alkalinity increased
 361 slightly and reached 1,952 mgCaCO₃/l in the last period (Figure 3). The ammonia concentration
 362 was constant at value of 143 mgN-NH₄⁺/l. The volatile fatty acids were completely consumed by
 363 methanogens and the concentration in the effluent was lower than 100 mgCOD/l. The utilisation of
 364 a co-substrate improved the stability of the process (pH, alkalinity and ammonium concentration),
 365 increased the volatile solids removal and, as confirmed by Fountoulakis et al. (2008) increased the
 366 methane production of 10-30%.

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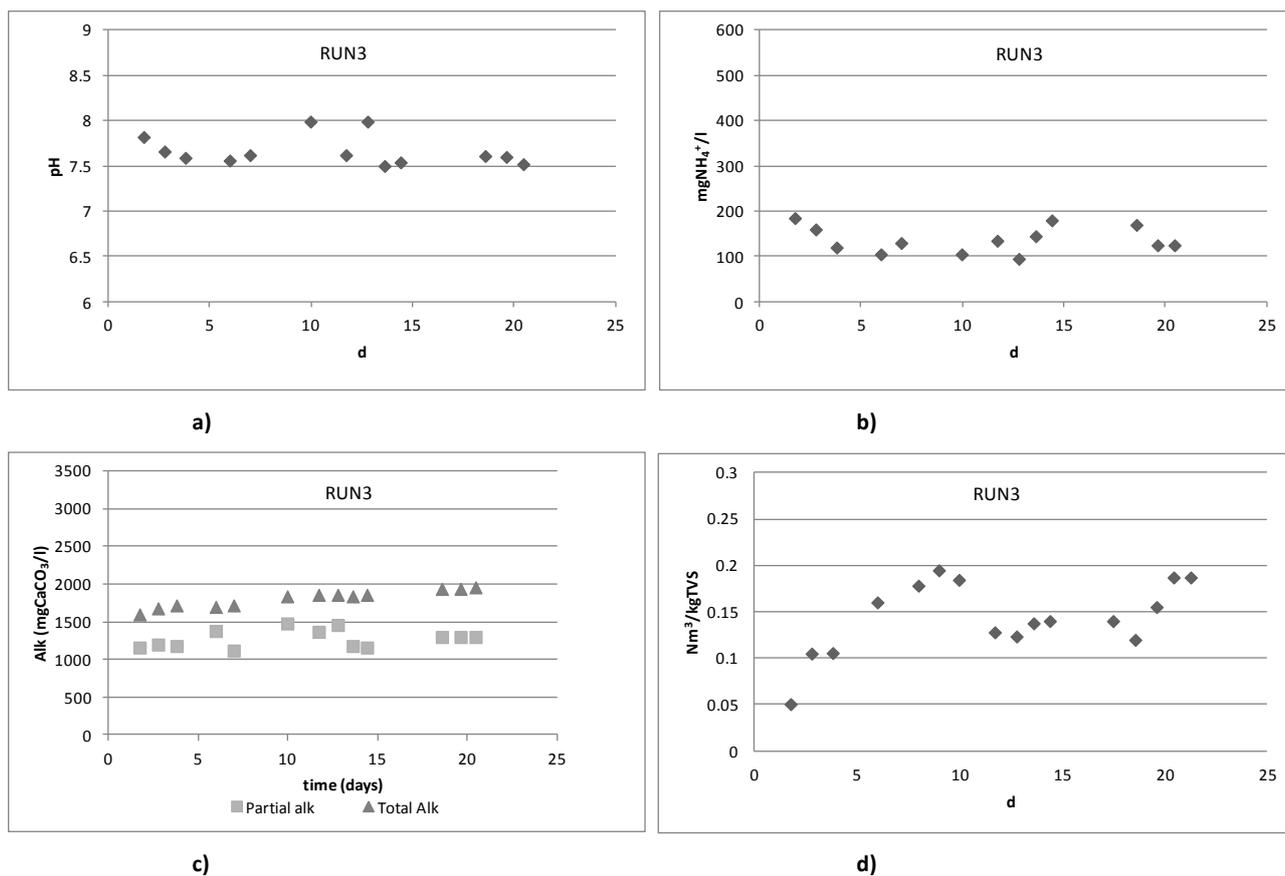


Figure 3. Trends of pH a), ammonia b), total and partial alkalinity c) SGP d), at OLR 4 kgVS/m³d (RUN3).

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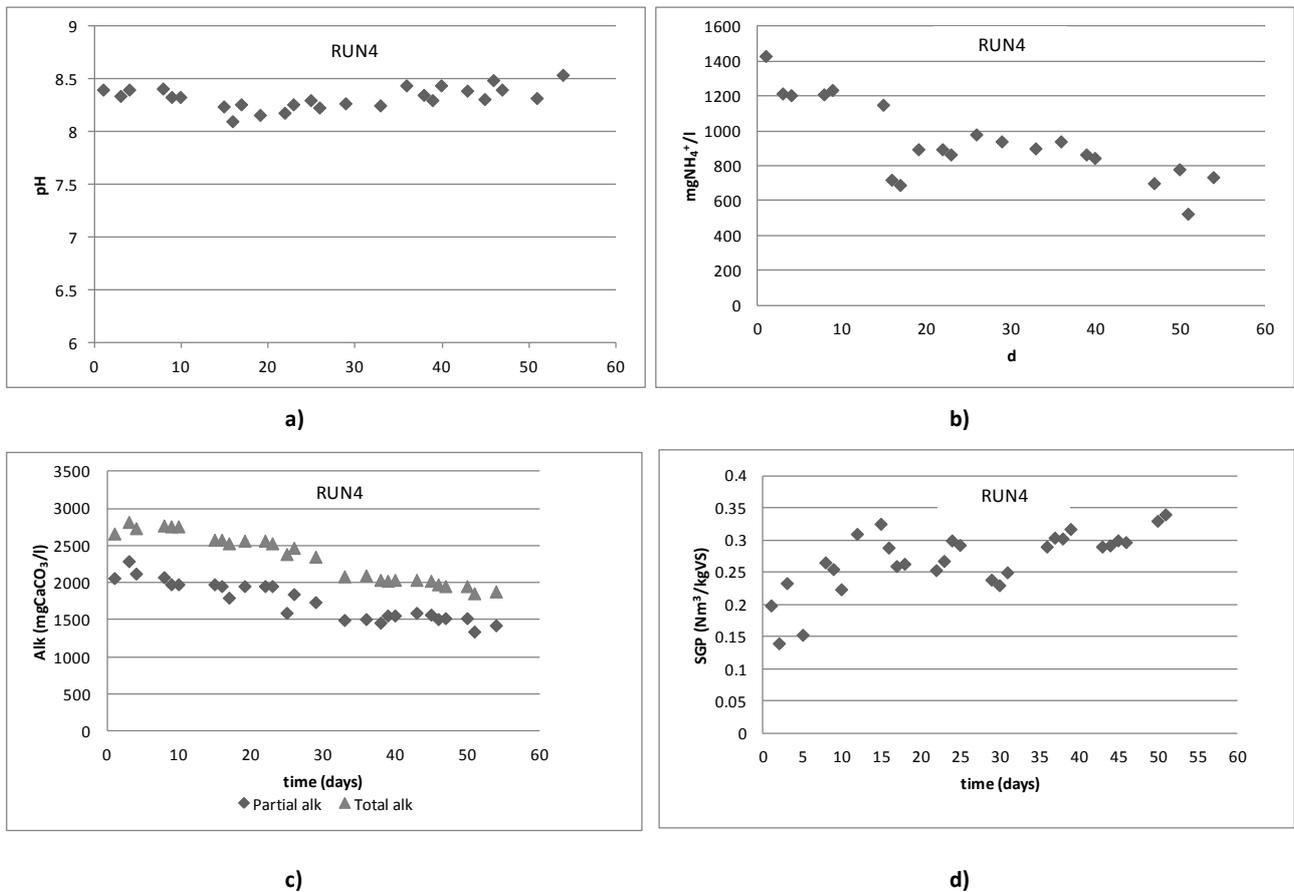
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373 Anyway the specific biogas production remained lower than value obtained by BMP tests, in order
374 to improve the degradation efficiency longer HRT was applied (RUN 4). Also a pre-treatment such
375 as fermentation could improve the biogas yield as reported by BMP of fermented GM. The effects
376 of these aspects were evaluated (RUN 4) with a reactor working with 1.2 gVS/l of OLR and 40
377 days of HRT, fed with fermented GM. Increasing the HRT, the flow rate was reduced from 250
378 ml/d to 125ml/d. Consequently the organic load decreased in order to maintain solid concentration
379 in the feed mixture comparable with RUN1 and RUN2.

380 The process was monitored for 55 days and reached stability after 35 days (Figure 4). The SGP was
381 0.290 Nm³/kgVS_{fed} with 61% of methane. The corresponding VS conversion into biogas was of
382 35%, higher than previous continuous trials because the long retention time and previous
383 fermentation promoted the hydrolysis of organic matter, however it was half of biodegradability
384 index obtained by batch test because of semi-continuous feeding mode. The biogas production
385 agrees with higher stability of the process. pH remained higher than 8 during the whole trial, this
386 value was explained by the higher concentration of ammonium in the digestate. In fact the
387 concentration at steady state was 734 mgN-NH₄⁺/l, significant major than in others examined
388 digestates, because of higher protein degradation. At the beginning the trend of alkalinity was

389 similar of those of the tests with VGM alone (Figure 3), but it stabilized on values 1,992
390 mgCaCO₃/l at steady state.

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Figure 4 Trends of pH a), ammonia b), total and partial alkalinity c) and SGP d), at OLR 1.2 kgVS/m³d (RUN4).

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In Table 5 the operational conditions, effluents characteristics and process yields are summarized. The effluents solids concentrations were affected by operational conditions, in particular the TS concentration increase with OLR. The VS/TS ratio and COD concentration reflected the substrates stabilisation: the reactor working with long HRT was characterized by lowest VS/TS percentage and lower COD content, due to higher organic matter conversion.

Comparing the SGP recorded during the continuous trials with VGM alone or with WAS, similar biogas production appeared but the percentage of methane was quite higher when only one substrate was used. The reason of different biogas composition could be due to organic matter composition of the feed, in particular grape marcs contained oil, compounds with higher theoretical methane production. Fermentation of GM duplicated the biogas production in agreement with BMP tests. Thermophilic digestion didn't seem to be more sensitive than mesophilic process, in fact no inhibition effects were detected. Anyway biogas production was comparable in the two operational temperature, consequently the higher cost of maintaining reactor at 55°C could be only justified by better hygienisation of effluent of co-digestion process.

Table 5 Comparison of operational conditions, effluents characteristics and specific yields of continuous trials

		RUN1	RUN2	RUN3	RUN4
Operational conditions					
V_r	l	5	5	5	5
HRT	d	20	20	20	40
OLR	gVS/l/d	1	2	4	1.2
Q	l/d	0.25	0.25	0.25	0.125
Effluent characteristics					
TS		35.6	41.0	55.1	55.0
VS		27.8	33.6	47.8	37.6
VS/TS	%	78	82	87	68
COD	mg/gTS	920.7	1083	981.2	889
pH	-	7.7	7.8	7.5	8.4
N-NH4	mgN-NH ₄ ⁺ /l	367.5	258.6	142.5	734
PA	mgCaCO ₃ /l	1,556	1,091	1,217	1,509
TA	mgCaCO ₃ /l	2,435	1,951	1,918	1,992
Yields					
SGP	Nm ³ /kgVS _{fed}	0.114	0.145	0.146	0.290
CH ₄	%	75%	76%	50%	61%
VS _{rem}	%	12%	15%	20%	35%

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413 3.5 Potential Energy recovery from Winery Waste production

414 The Italian, European and worldwide winery wastes production was calculated considering the wine
 415 production of 2013 and the specific production factor reported by ANPA (2001). The GM
 416 represented the 65% of whole organic waste production by winery sector (Table 5) and the recent
 417 legislation encourages its use to energy production.

418 Considering this biogas yield and the production of GM in Italy, in Europe and around the World,
 419 the evaluation of potential energy from this by-product was calculated. If the biogas produced is
 420 exploited using CHP units, with thermal efficiency of 50% and electrical efficiency of 35%, the
 421 energy produced would be a great deal (Table 6). The heat energy reported in Table 6 is a net value,
 422 subtracting the thermal energy used for biomass and digesters heating, then the process could be
 423 energetically self-sustaining. Assuming same biogas yields operating at 37°C the available heat
 424 increased of 8%.

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Table 6 Production of grape marcs, grape stalks and wine lees in 2011

	Wine	GM	GS	WL
	MHI	Thousands of Tons		
Italy	44.9	808.2	179.6	269.4
Europe	164.2	2,955.6	656.8	985.2
World	278.6	5,014.8	1,114.4	1,671.6

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Table 7 Production of grape marcs and corresponding heat and electricity production

	GM	Thermal Energy	Electricity
	10 ³ tons	GWh/y	GWh/y
Italy	808.2	245	201
Europe	2,955.6	896	734
World	5,014.8	1,520	1,245

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429 The gain obtained from selling the electric energy depends by the incentives applied, but even
 430 considering average plant size smaller than 1MWh the minimum price for 2014 is 174.4 €/MWh
 431 (DM July 6th, 2012), it is possible to obtain about 35,054,400 €/y just in Italy.

432 4. Conclusions

433 Thermophilic batch test were carried out with different winery waste and the results of BMP tests
 434 showed specific methane production of 0.150-0.301 Nm³CH₄/kgVS_{fed} for virgin and fermented
 435 grape marcs, 0.121 Nm³/kgVS_{fed} for grape stalks and 0.216 Nm³CH₄/kgVS_{fed} for wine lees. The
 436 specific methane production were similar with those reported in literature at 37°C. The kinetic study
 437 demonstrated that modified Gompertz model well fitted (R² 0.99-1.00) the methane production
 438 cumulative curve in case of presence of lag phase at the beginning of the test. While the anaerobic
 439 degradation of virgin grape marcs was better described by first order equation (R² 0.99). The
 440 determined specific yields and kinetic parameters were comparable with one at 37°C.

441 AD semi-continuous trials of GM were characterized by low biogas production (0.114-0.145
 442 Nm³/kgVS_{fed}). The addition of waste activated sludge improve process stability but didn't increased
 443 biodegradation of substrate. The biogas production increased with fermented grape marcs and
 444 applying longer HRT (40 d) obtaining 0.29 Nm³/kgVS_{fed}; the effluent had lower COD content due
 445 to higher organic matter degradation (35% of volatile solids).

446 Considering best biogas yields, the potential electricity and heat were calculated using a typical
447 CHP unit efficiency. The combustion of biogas generated by GM could generate, in whole world,
448 1520 GWh/year of heat and 1245 GWh/year of electricity that could be used in cellar facilities.
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